# System Identification

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# Part VIII

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#### Recall **taxonomy of models** from Part I:

By number of parameters:

- <sup>1</sup> Parametric models: have a fixed form (mathematical formula), with a known, often small number of parameters
- <sup>2</sup> Nonparametric models: cannot be described by a fixed, small number of parameters Often represented as graphs or tables

#### By amount of prior knowledge ("color"):

- <sup>1</sup> First-principles, white-box models: fully known in advance
- 2 Black-box models: entirely unknown
- **3** Gray-box models: partially known

<span id="page-3-0"></span>Like prediction error methods, instrumental variable methods produce *black-box*, *parametric*, polynomial models.



- The ARX method is simple (linear regression), but only supports limited classes of disturbance
- **General PEM supports any (reasonable) disturbance,** but it is relatively difficult to apply from a numerical point of view

Can we come up with a method that combines both advantages?

### (qualified) **Yes! Instrumental variables**

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### Recall: ARX model

$$
A(q^{-1})y(k) = B(q^{-1})u(k) + e(k)
$$
  

$$
(1+a_1q^{-1} + \dots + a_{na}q^{-na})y(k) =
$$
  

$$
(b_1q^{-1} + \dots + b_{nb}q^{-nb})u(k) + e(k)
$$

<span id="page-6-0"></span>

### ARX model: explicit form and detailed diagram

In explicit form:

$$
y(k) = -a_1y(k-1) - a_2y(k-2) - \ldots - a_{na}y(k-na) b_1u(k-1) + b_2u(k-2) + \ldots + b_{nb}u(k-nb) + e(k)
$$

where the model parameters are:  $a_1, a_2, \ldots, a_{n_a}$  and  $b_1, b_2, \ldots, b_{nb}$ .



### Recall: Linear regression representation

$$
y(k) = \begin{bmatrix} -y(k-1) & \cdots & -y(k-na) & u(k-1) & \cdots & u(k-nb) \end{bmatrix}
$$

$$
\begin{bmatrix} a_1 & \cdots & a_{na} & b_1 & \cdots & b_{nb} \end{bmatrix}^\top + e(k)
$$

$$
=:\varphi^\top(k)\theta + e(k)
$$

Regressor vector:  $\varphi \in \mathbb{R}^{n\alpha + nb}$ , previous output and input values. Parameter vector:  $\theta \in \mathbb{R}^{n\alpha+nb}$ , polynomial coefficients.

#### [Analytical development of IV methods](#page-3-0) [Matlab example](#page-26-0) [Theoretical guarantees](#page-32-0) [Closed-loop identification using IV](#page-37-0) [Closed-loop Matlab example](#page-44-0) 000000 0000000 Recall: Identification problem and solution

Given dataset  $u(k)$ ,  $y(k)$ ,  $k = 1, \ldots, N$ , find model parameters  $\theta$  to achieve small errors ε(*k*) in:

$$
y(k) = \varphi^\top(k)\theta + \varepsilon(k)
$$

Formal objective: minimize the mean squared error:

$$
V(\theta) = \frac{1}{N} \sum_{k=1}^{N} \varepsilon(k)^2
$$

Solution: can be written in several ways, here we use:

$$
\widehat{\theta} = \left[ \frac{1}{N} \sum_{k=1}^{N} \varphi(k) \varphi^{T}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^{N} \varphi(k) y(k) \right]
$$

### Parameter errors

Finally, recall that for the guarantees, a true parameter vector  $\theta_0$  is assumed to exist:

$$
y(k) = \varphi^\top(k)\theta_0 + v(k)
$$

Analyze the parameter errors (a vector of *n* elements):

$$
\widehat{\theta} - \theta_0 = \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) \varphi^{\top}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) y(k) \right]
$$

$$
- \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) \varphi^{\top}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) \varphi^{\top}(k) \right] \theta_0
$$

$$
= \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) \varphi^{\top}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) [y(k) - \varphi^{\top}(k) \theta_0] \right]
$$

$$
= \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) \varphi^{\top}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^N \varphi(k) v(k) \right]
$$



We wish the algorithm to be consistent: the parameter errors should become 0 in the limit of infinite data (and they should be well-defined).

As 
$$
N \to \infty
$$
:  
\n
$$
\frac{1}{N} \sum_{k=1}^{N} \varphi(k) \varphi^{T}(k) \to E \{ \varphi(k) \varphi^{T}(k) \}
$$
\n
$$
\frac{1}{N} \sum_{k=1}^{N} \varphi(k) v(k) \to E \{ \varphi(k) v(k) \}
$$

For the error to be (1) well-defined and (2) equal to zero, we need:

- **D** E $\{\varphi(k)\varphi^{\top}(k)\}$  invertible.
- 2 E { $\varphi(k)$ *v*(*k*)} zero.

### White noise required

- We have  $E\{\varphi(k) v(k)\} = 0$  if the elements of  $\varphi(k)$  are uncorrelated with *v*(*k*) (note that *v*(*k*) is assumed zero-mean).
- $\bullet$  But  $\varphi(k)$  includes  $y(k-1), y(k-2), \ldots$ , which depend on  $v(k-1), v(k-2), \ldots$
- So the only option is to have  $v(k)$  uncorrelated with  $v(k-1)$ ,  $v(k-2)$ , ...  $\Rightarrow v(k)$  must be *white noise*.

Instrumental variables are a solution to remove this limitation to white noise.

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$$
\widehat{\theta} - \theta_0 = \left[ \frac{1}{N} \sum_{k=1}^{N} \varphi(k) \varphi^{T}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^{N} \varphi(k) v(k) \right]
$$

1

Idea: What if a different vector than  $\varphi(k)$  could be included in the product with *v*(*k*)?

$$
\widehat{\theta} - \theta_0 = \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{T}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) v(k) \right]
$$

where the elements of  $Z(k)$  are uncorrelated with  $v(k)$ . Then  $E\left\{Z(k)v(k)\right\}=0$  and the error can be zero.

Vector *Z*(*k*) has *n* elements, which are called instruments.

### Instrumental variable method

In order to have:

<span id="page-15-2"></span>
$$
\widehat{\theta} - \theta_0 = \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{T}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) v(k) \right]
$$
(8.1)

the estimated parameter must be:

<span id="page-15-1"></span>
$$
\widehat{\theta} = \left[\frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{T}(k)\right]^{-1} \left[\frac{1}{N} \sum_{k=1}^{N} Z(k) y(k)\right]
$$
(8.2)

This  $\widehat{\theta}$  is the solution to the system of *n* equations:

<span id="page-15-0"></span>
$$
\left[\frac{1}{N}\sum_{k=1}^{N}Z(k)\varphi^{\top}(k)\right]\theta=\left[\frac{1}{N}\sum_{k=1}^{N}Z(k)y(k)\right]
$$
(8.3)

Constructing and solving this system gives the basic instrumental variable (IV) method.

### Instrumental variable method: Alternate form

Alternate form of the system of equations::

<span id="page-16-0"></span>
$$
\left[\frac{1}{N}\sum_{k=1}^{N}Z(k)[\varphi^{\top}(k)\theta-\gamma(k)]\right]=0
$$
\n(8.4)

Exercise: Show that [\(8.4\)](#page-16-0) is equivalent to [\(8.3\)](#page-15-0), and that they imply [\(8.2\)](#page-15-1), which in turn implies [\(8.1\)](#page-15-2).



So far the instruments *Z*(*k*) were not discussed. They are usually created based on the inputs (including outputs would lead to correlation with *v* and so eliminate the advantage of IV).

Simple possibility: just include additional delayed inputs to obtain a vector of the appropriate size,  $n = na + nb$ :

 $Z(k) = [u(k - nb - 1), \ldots u(k - na - nb), u(k - 1), \ldots, u(k - nb)]^{\top}$ 

Compare to original vector:

 $\varphi(k) = [-\gamma(k-1), \ldots, -\gamma(k-na), u(k-1), \ldots, u(k-nb)]^\top$ 

Question: Why not just include  $u(k - 1), \ldots, u(k - na)$ ?



Take *na* past values from generic instrumental variable *x*:

$$
Z(k) = [-x(k-1),..., -x(k-na), u(k-1),..., u(k-nb)]^{\top}
$$

which is the output of a transfer function with *u* at the input:

$$
C(q^{-1})x(k)=D(q^{-1})u(k)
$$

Remark:  $C(q^{-1})$ ,  $D(q^{-1})$  have different meanings than in PEM.

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$$
(1 + c_1q^{-1} + \cdots + c_{nb}q^{-nc})x(k) =
$$
  
\n
$$
(d_1q^{-1} + \cdots + d_{nd}q^{-nd})u(k)
$$
  
\n
$$
x(k) = -c_1x(k-1) - c_2x(k-2) - \cdots - c_{nc}x(k-nc)
$$
  
\n
$$
+ d_1u(k-1) + d_2u(k-2) + \cdots + d_{nd}u(k-nd)
$$



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In order to obtain:

$$
Z(k) = [u(k - nb - 1), \ldots u(k - na - nb), u(k - 1), \ldots, u(k - nb)]^{\top}
$$

set *C* = 1, *D* = −*q* −*nb* .

Exercise: Verify that the desired *Z*(*k*) is indeed obtained.

### Generalized instruments: Initial model

Generalized instruments:

 $Z(k) = [-x(k-1), \ldots, -x(k-na), u(k-1), u(k-2), \ldots, u(k-nb)]^{\top}$ 

Compare to original vector:

 $\varphi(k) = [-y(k-1), \ldots, -y(k-na), u(k-1), \ldots, u(k-nb)]^\top$ 

Idea: Take instrument generator equal to an initial model,  $C(q^{-1}) = A(q^{-1}), D(q^{-1}) = B(q^{-1}).$  This model can be obtained e.g. with ARX estimation.

The instruments are an approximation of *y*:

 $Z(k) = [-\hat{y}(k-1), \ldots - \hat{y}(k-na), u(k-1), \ldots, u(k-nb)]$ that has the crucial advantage of being *uncorrelated* with the noise. Note here  $\hat{v}$  is the *simulated* output!

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# IV method summary

#### IV method

- 1: **for** each step  $k = 1, 2, ..., N$  **do**
- 2: form regressor vector:

$$
\varphi(k) = [-y(k-1),\cdots,-y(k-na),u(k-1),\cdots,u(k-nb)]^{\top}
$$

3: form IV vector:  
\n
$$
Z(k) = [-x(k-1), \cdots, -x(k-na), u(k-1), \cdots, u(k-nb)]^{\top}
$$
\n4: simulate IV operator:  $x(k) = Z^{\top}(k)[C_1, \cdots, C_2, d_1, \cdots, d_n]^{\top}$ 

- 4: simulate IV generator:  $x(k) = Z^{\top}(k)[c_1, \cdots, c_{nc}, d_1, \cdots, d_{nd}]$
- 5: **end for**
- 6: compute  $\tilde{\Phi} = \frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{\top}(k)$ , an  $(na + nb) \times (na + nb)$  matrix
- 7: compute  $\tilde{Y} = \frac{1}{N} \sum_{k=1}^{N} Z(k) y(k)$ , an  $na + nb$  vector
- 8: solve  $\tilde{\Phi}\theta = \tilde{Y}$
- 9:  $\textsf{return } \theta = [a_1, \ldots, a_{na}, b_1, \ldots, b_{nb}]^\top$

Negative-time signals set to 0 as usual.

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Both PEM and IV can be seen as extensions of ARX:

$$
A(q^{-1})y(k) = B(q^{-1})u(k) + e(k)
$$

to disturbances *v*(*k*) different from white noise *e*(*k*).



- PEM explicitly include the disturbance model in the structure, e.g. in ARMAX  $v(k) = C(q^{-1})e(k)$  leading to  $A(q^{-1})y(k) = B(q^{-1})u(k) + C(q^{-1})e(k).$
- IV methods do *not* explicitly model the disturbance, but are designed to be resilient to non-white, "colored" disturbance, by using instruments *Z*(*k*) uncorrelated with it.

Comparison (continued)

Advantage of IV: Simple model structure, identification consists only of solving a system of linear equations. In contrast, PEM required solving optimization problems with e.g. Newton's method, was susceptible to local minima etc.

Disadvantage of IV (why it was only a *qualified* yes in the beginning): In practice, for finite number *N* of data, model quality depends heavily on the choice of instruments  $Z(k)$ . Moreover, the resulting model has a larger risk of being unstable (even for a stable real system).

Methods exist to choose instruments  $Z(k)$  that are optimal in a certain sense, but they will not be discussed here.

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From prior knowledge, the system has order 2 and the disturbance is colored (does not obey the ARX model structure).

Remarks: As before, the identification input is a pseudo-random binary signal, and the validation input a sequence of steps.



### IV identification with custom instruments

Define the instruments by the generating transfer function, using polynomials  $C(q^{-1})$  and  $D(q^{-1})$ .

 $model = iv(id, [na, nb, nk], C, D);$ 

Arguments:

- **D** Identification data.
- <sup>2</sup> Array containing the orders of *A* and *B* and the delay *nk* (like for ARX).
- <sup>3</sup> Polynomials *C* and *D*, as vectors of coefficients in increasing power of  $q^{-1}$ .

### Result with simple instruments

Take  $C(q^{-1})=1$ ,  $D(q^{-1})=-q^{-nb}$ , leading to  $Z(k) = [u(k - nb - 1), \ldots u(k - na - nb), u(k - 1), \ldots, u(k - nb)]^{\top}$ . Compare to ARX.



#### Conclusions:

- Model unstable  $\Rightarrow$  in general, must pay attention because IV models are not guaranteed to be stable! (recall the Comparison)
- Results very bad with this simple choice.

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### Result with ARX-model instruments



Conclusion: IV obtains better results. This is because the disturbance is colored, and IV can deal effectively with this case (whereas ARX cannot – but it still provides a useful starting point for IV).

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 $model = iv4(id, [na, nb, nk]);$ 

Implements an algorithm that generates near-optimal instruments.



Conclusion: Virtually the same performance as ARX instruments.



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#### Assumptions

#### Assumptions (simplified)

- <sup>1</sup> The disturbance *v*(*k*) = *H*(*q* −1 )*e*(*k*) where *e*(*k*) is zero-mean white noise, and  $H(q^{-1})$  is a transfer function satisfying certain conditions.
- <sup>2</sup> The input signal *u*(*k*) has a sufficiently large order of PE and does not depend on the disturbance (the experiment is open-loop).
- <sup>3</sup> The real system is stable and *uniquely* representable by the model chosen: there exists exactly one  $\theta_0$  so that polynomials  $\mathcal{A}(q^{-1}; \theta_0)$  and  $\mathcal{B}(q^{-1}; \theta_0)$  are identical to those of the real system.
- **•** Matrix  $E\left\{Z(k)Z^{\top}(k)\right\}$  is invertible.

### Discussion of assumptions

- Assumption 1 shows the main advantage of IV over PEM: the disturbance can be colored.
- Assumptions 2 and 3 are not very different from those made by PEM. Stability of a discrete-time system requires its poles to be strictly inside the unit circle:



Question: Why is the experiment not allowed to be closed-loop?

Assumption 4 is required to solve the linear system, and given an input with sufficient order of PE boils down to an appropriate selection of instruments (e.g. not repeating the same delayed input  $u(k - i)$  twice).

### **Guarantee**

#### Theorem 1

As the number of data points  $N \to \infty$ , the solution  $\widehat{\theta}$  of IV estimation converges to the true parameter vector  $\theta_0$ .

Remark: This is a consistency guarantee, in the limit of infinitely many data points.

### Possible extensions

- Multiple-input, multiple-output systems.
- **Larger-dimension instruments Z than parameter vectors**  $\theta$ with other modifications, called extended IV methods.
- Identification of systems operating in closed loop: next

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In practice, systems must often be controlled, because when they operate on their own, in open loop:

- They would be unstable
- Safety or economical limits for the signals would not be satisfied

This means that *u*(*k*) is computed using feedback from *y*(*k*): the system operates in closed loop

### Closed-loop identification

However, most of the techniques that we studied assume the system functions in open loop! For instance, IV guarantees require (among other things):

#### $\bullet$  ...

- The input signal *u*(*k*) does not depend on the disturbance (the experiment is open-loop)
- ...

Removing this condition leads to **closed-loop identification**.

Several techniques can be modified for this setting, notably including prediction error methods.

Here, we will focus on IV methods since they are easy to modify.

### Closed-loop IV structure



$$
A(q^{-1})y(k) = B(q^{-1})u(k) + v(k)
$$
  

$$
u(k) = \mathcal{K}(q^{-1})(r(k) - y(k))
$$

where  $\mathcal{K}(q^{-1})$  is the transfer function of the controller, and  $r(k)$  is a reference signal

Therefore, *u*(*k*) dynamically depends both on the reference signal and on the system output



The open-loop condition will of course fail. Let us dig deeper into it. The underlying reason for which we needed the loop open was to make the parameter errors:

$$
\widehat{\theta} - \theta_0 = \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{T}(k) \right]^{-1} \left[ \frac{1}{N} \sum_{k=1}^{N} Z(k) v(k) \right]
$$

equal to zero, leading to a good model. For this, we require:

- $\bullet$  E { $Z(k)v(k)$ } zero.
- $\mathrm{E}\left\{Z(k)\varphi^{\top}(k)\right\}$  invertible.

With the usual IV choices, computed based on *u* (which now depends on *y* and hence on *v*), the first condition would fail.

The vector of IVs *Z*(*k*) is not allowed to depend on *u*(*k*) anymore.

Idea: **make it a function of** *r*(*k*)!

Then:

- $\bullet$  E { $Z(k)v(k)$ } will naturally be zero, since we are the ones generating the reference *r*, independently from the disturbance *v*
- We can make  $\text{E}\left\{Z(k)\varphi^{\top}(k)\right\}$  invertible by ensuring the IVs are good (e.g. no linear dependence), and that the reference *r* has a sufficiently high order of PE



Simplest idea – include in *Z* the appropriate number of delayed reference values:

$$
Z(k) = [r(k-1), r(k-2), \ldots r(k-na-nb)]^{\top}
$$

Slightly generalized to linear combinations of these values:

$$
Z(k) = F \cdot [r(k-1), r(k-2), \ldots r(k-na-nb)]^{\top}
$$

where *F* is invertible. The simple case is recovered by taking *F* the identity matrix.

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### Experimental data

#### Identification left, and validation right:



Similarly to the open-loop case, the system has order 2 and the disturbance is colored (does not obey the ARX model structure).

However, now the input is generated by a controller based on the reference signal *r*, which is a PRBS.

## **Results**



- Regular IV with ARX instruments: fails.
- Closed-loop IV using *r* to generate instruments: works.



- Objective: combine simplicity of ARX linear regression with generality of PEM disturbance *v*
- Examined in-depth why ARX fails for colored disturbance *v*
- Solution: replace regressors  $\varphi$  (at strategic places in equations) by *instrumental variables Z* that do not depend on *y*
- Several ways to compute *Z* from *u* only
- Solution quality dependent on Z, may even be unstable
- Matlab example
- Further generalizing *Z* to depend only on reference *r* allows IV to work in closed-loop
- Matlab example for closed-loop identification