System Identification

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Part VIII

Instrumental variable methods. Closed-loop identification

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Recall taxonomy of models from Part I:

By number of parameters:

- Parametric models: have a fixed form (mathematical formula), with a known, often small number of parameters
- Nonparametric models: cannot be described by a fixed, small number of parameters Often represented as graphs or tables

By amount of prior knowledge ("color"):

- Sirst-principles, white-box models: fully known in advance
- Black-box models: entirely unknown
- Gray-box models: partially known

Like prediction error methods, instrumental variable methods produce *black-box*, *parametric*, polynomial models.

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 Overall motivation
 Overall motivatio

- The ARX method is simple (linear regression), but only supports limited classes of disturbance
- General PEM supports any (reasonable) disturbance, but it is relatively difficult to apply from a numerical point of view

Can we come up with a method that combines both advantages?

(qualified) Yes! Instrumental variables

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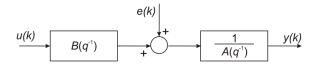
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Recall: ARX model

$$A(q^{-1})y(k) = B(q^{-1})u(k) + e(k)$$

(1+a₁q⁻¹ + ... + a_{na}q^{-na})y(k) =
(b₁q⁻¹ + ... + b_{nb}q^{-nb})u(k) + e(k)



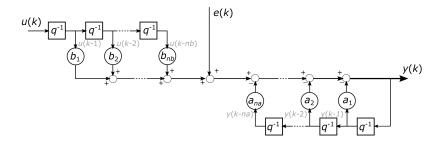
ARX model: explicit form and detailed diagram

In explicit form:

$$y(k) = -a_1y(k-1) - a_2y(k-2) - \dots - a_{na}y(k-na)$$

$$b_1u(k-1) + b_2u(k-2) + \dots + b_{nb}u(k-nb) + e(k)$$

where the model parameters are: $a_1, a_2, \ldots, a_{n_a}$ and b_1, b_2, \ldots, b_{nb} .



Recall: Linear regression representation

$$y(k) = \begin{bmatrix} -y(k-1) & \cdots & -y(k-na) & u(k-1) & \cdots & u(k-nb) \end{bmatrix}$$
$$\cdot \begin{bmatrix} a_1 & \cdots & a_{na} & b_1 & \cdots & b_{nb} \end{bmatrix}^\top + e(k)$$
$$=: \varphi^\top(k)\theta + e(k)$$

Regressor vector: $\varphi \in \mathbb{R}^{na+nb}$, previous output and input values. Parameter vector: $\theta \in \mathbb{R}^{na+nb}$, polynomial coefficients.

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Given dataset u(k), y(k), k = 1, ..., N, find model parameters θ to achieve small errors $\varepsilon(k)$ in:

$$\mathbf{y}(\mathbf{k}) = \varphi^{\top}(\mathbf{k})\theta + \varepsilon(\mathbf{k})$$

Formal objective: minimize the mean squared error:

$$V(heta) = rac{1}{N}\sum_{k=1}^N arepsilon(k)^2$$

Solution: can be written in several ways, here we use:

$$\widehat{\theta} = \left[\frac{1}{N}\sum_{k=1}^{N}\varphi(k)\varphi^{\top}(k)\right]^{-1}\left[\frac{1}{N}\sum_{k=1}^{N}\varphi(k)y(k)\right]$$

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Parameter errors

Finally, recall that for the guarantees, a true parameter vector θ_0 is assumed to exist:

$$\mathbf{y}(\mathbf{k}) = \varphi^{ op}(\mathbf{k}) \mathbf{ heta}_0 + \mathbf{v}(\mathbf{k})$$

Analyze the parameter errors (a vector of *n* elements):

$$\widehat{\theta} - \theta_0 = \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^{\mathsf{T}}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\mathbf{y}(k)\right] \\ - \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^{\mathsf{T}}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^{\mathsf{T}}(k)\right] \theta_0 \\ = \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^{\mathsf{T}}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)[\mathbf{y}(k) - \varphi^{\mathsf{T}}(k)\theta_0]\right] \\ = \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^{\mathsf{T}}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\mathbf{v}(k)\right]$$



We wish the algorithm to be consistent: the parameter errors should become 0 in the limit of infinite data (and they should be well-defined).

As
$$N \to \infty$$
:

$$\frac{1}{N} \sum_{k=1}^{N} \varphi(k) \varphi^{\top}(k) \to \mathrm{E} \left\{ \varphi(k) \varphi^{\top}(k) \right\}$$

$$\frac{1}{N} \sum_{k=1}^{N} \varphi(k) v(k) \to \mathrm{E} \left\{ \varphi(k) v(k) \right\}$$

For the error to be (1) well-defined and (2) equal to zero, we need:

- E { $\varphi(k)\varphi^{\top}(k)$ } invertible.
- 2 $E \{\varphi(k)v(k)\}$ zero.

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White noise required

- We have E {φ(k)v(k)} = 0 if the elements of φ(k) are uncorrelated with v(k) (note that v(k) is assumed zero-mean).
- But $\varphi(k)$ includes $y(k-1), y(k-2), \ldots$, which depend on $v(k-1), v(k-2), \ldots$!
- So the only option is to have v(k) uncorrelated with $v(k-1), v(k-2), \ldots \Rightarrow v(k)$ must be *white noise*.

Instrumental variables are a solution to remove this limitation to white noise.

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|--------------------------------------|----------------|------------------------|-------------------------------------|----------------------------|
| Intuition | | | | |

$$\widehat{\theta} - \theta_0 = \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)\varphi^\top(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N \varphi(k)v(k)\right]$$

Idea: What if a different vector than $\varphi(k)$ could be included in the product with v(k)?

$$\widehat{\theta} - \theta_0 = \left[\frac{1}{N}\sum_{k=1}^N Z(k)\varphi^{\top}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N Z(k)v(k)\right]$$

where the elements of Z(k) are uncorrelated with v(k). Then E {Z(k)v(k)} = 0 and the error can be zero.

Vector Z(k) has *n* elements, which are called instruments.

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Instrumental variable method

In order to have:

$$\widehat{\theta} - \theta_0 = \left[\frac{1}{N}\sum_{k=1}^N Z(k)\varphi^{\top}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N Z(k)v(k)\right]$$
(8.1)

the estimated parameter must be:

$$\widehat{\theta} = \left[\frac{1}{N}\sum_{k=1}^{N} Z(k)\varphi^{\top}(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^{N} Z(k)y(k)\right]$$
(8.2)

This $\hat{\theta}$ is the solution to the system of *n* equations:

$$\left[\frac{1}{N}\sum_{k=1}^{N}Z(k)\varphi^{\top}(k)\right]\theta = \left[\frac{1}{N}\sum_{k=1}^{N}Z(k)y(k)\right]$$
(8.3)

Constructing and solving this system gives the basic instrumental variable (IV) method.

Instrumental variable method: Alternate form

Alternate form of the system of equations::

$$\left[\frac{1}{N}\sum_{k=1}^{N}Z(k)[\varphi^{\top}(k)\theta - y(k)]\right] = 0$$
(8.4)

Exercise: Show that (8.4) is equivalent to (8.3), and that they imply (8.2), which in turn implies (8.1).

So far the instruments Z(k) were not discussed. They are usually created based on the inputs (including outputs would lead to correlation with v and so eliminate the advantage of IV).

Simple possibility: just include additional delayed inputs to obtain a vector of the appropriate size, n = na + nb:

 $Z(k) = [u(k - nb - 1), \dots u(k - na - nb), u(k - 1), \dots, u(k - nb)]^{\top}$

Compare to original vector:

 $\varphi(k) = \left[-y(k-1), \ldots, -y(k-na), u(k-1), \ldots, u(k-nb)\right]^{\top}$

Question: Why not just include $u(k - 1), \ldots, u(k - na)$?

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Generalization

Take *na* past values from generic instrumental variable *x*:

 $Z(k) = [-x(k-1), \dots, -x(k-na), u(k-1), \dots, u(k-nb)]^{\top}$

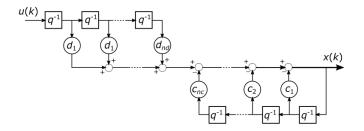
which is the output of a transfer function with u at the input:

$$C(q^{-1})x(k) = D(q^{-1})u(k)$$

Remark: $C(q^{-1})$, $D(q^{-1})$ have different meanings than in PEM.

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$$(1 + c_1 q^{-1} + \dots + c_{nb} q^{-nc}) x(k) = (d_1 q^{-1} + \dots + d_{nd} q^{-nd}) u(k) x(k) = -c_1 x(k-1) - c_2 x(k-2) - \dots - c_{nc} x(k-nc) + d_1 u(k-1) + d_2 u(k-2) + \dots + d_{nd} u(k-nd)$$



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 Generalized instruments: obtaining the simple case

In order to obtain:

$$Z(k) = [u(k - nb - 1), \dots u(k - na - nb), u(k - 1), \dots, u(k - nb)]^{\top}$$

set C = 1, $D = -q^{-nb}$.

Exercise: Verify that the desired Z(k) is indeed obtained.

Generalized instruments: Initial model

Generalized instruments:

 $Z(k) = [-x(k-1), \dots, -x(k-na), u(k-1), u(k-2), \dots, u(k-nb)]^{\top}$

Compare to original vector:

 $\varphi(k) = \left[-y(k-1), \ldots, -y(k-na), u(k-1), \ldots, u(k-nb)\right]^{\top}$

Idea: Take instrument generator equal to an initial model, $C(q^{-1}) = \widehat{A}(q^{-1}), D(q^{-1}) = \widehat{B}(q^{-1})$. This model can be obtained e.g. with ARX estimation.

The instruments are an approximation of *y*:

 $Z(k) = \left[-\hat{y}(k-1), \dots - \hat{y}(k-na), u(k-1), \dots, u(k-nb)\right]^{\perp}$ that has the crucial advantage of being *uncorrelated* with the noise. Note here \hat{y} is the *simulated* output!

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IV method summary

IV method

3:

- 1: for each step $k = 1, 2, \ldots, N$ do
- 2: form regressor vector:

$$\varphi(k) = [-y(k-1), \cdots, -y(k-na), u(k-1), \cdots, u(k-nb)]^{\top}$$

form IV vector:

$$Z(k) = [-x(k-1), \dots, -x(k-na), u(k-1), \dots, u(k-nb)]^{\top}$$
simulate IV generator: $x(k) = Z^{\top}(k)[a - a - d - d - d]^{\top}$

4: simulate IV generator: $x(k) = Z^{+}(k)[c_1, \cdots, c_{nc}, d_1, \cdots, d_{nd}]$

5: end for

- 6: compute $\tilde{\Phi} = \frac{1}{N} \sum_{k=1}^{N} Z(k) \varphi^{\top}(k)$, an $(na+nb) \times (na+nb)$ matrix
- 7: compute $\tilde{Y} = \frac{1}{N} \sum_{k=1}^{N} Z(k) y(k)$, an na + nb vector
- 8: solve $\tilde{\Phi}\theta = \tilde{Y}$
- 9: return $\theta = [a_1, \ldots, a_{na}, b_1, \ldots, b_{nb}]^\top$

Negative-time signals set to 0 as usual.

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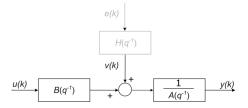
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Both PEM and IV can be seen as extensions of ARX:

$$A(q^{-1})y(k) = B(q^{-1})u(k) + e(k)$$

to disturbances v(k) different from white noise e(k).



- PEM explicitly include the disturbance model in the structure, e.g. in ARMAX $v(k) = C(q^{-1})e(k)$ leading to $A(q^{-1})y(k) = B(q^{-1})u(k) + C(q^{-1})e(k).$
- IV methods do not explicitly model the disturbance, but are designed to be resilient to non-white, "colored" disturbance, by using instruments Z(k) uncorrelated with it.

Closed-loop identification using IV

Comparison (continued)

Advantage of IV: Simple model structure, identification consists only of solving a system of linear equations. In contrast, PEM required solving optimization problems with e.g. Newton's method, was susceptible to local minima etc.

Disadvantage of IV (why it was only a *qualified* yes in the beginning): In practice, for finite number N of data, model quality depends heavily on the choice of instruments Z(k). Moreover, the resulting model has a larger risk of being unstable (even for a stable real system).

Methods exist to choose instruments Z(k) that are optimal in a certain sense, but they will not be discussed here.

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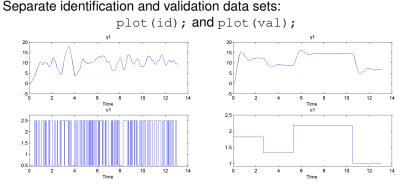
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From prior knowledge, the system has order 2 and the disturbance is colored (does not obey the ARX model structure).

Remarks: As before, the identification input is a pseudo-random binary signal, and the validation input a sequence of steps.

IV identification with custom instruments

```
Define the instruments by the generating transfer function, using polynomials C(q^{-1}) and D(q^{-1}).
model = iv(id, [na, nb, nk], C, D);
```

Arguments:

- Identification data.
- Array containing the orders of A and B and the delay nk (like for ARX).
- Polynomials C and D, as vectors of coefficients in increasing power of q⁻¹.

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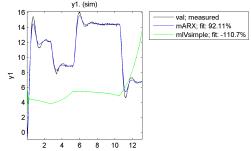
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Result with simple instruments

Take $C(q^{-1}) = 1$, $D(q^{-1}) = -q^{-nb}$, leading to $Z(k) = [u(k - nb - 1), \dots, u(k - na - nb), u(k - 1), \dots, u(k - nb)]^{\top}$. Compare to ARX.



Conclusions:

- Model unstable ⇒ in general, must pay attention because IV models are not guaranteed to be stable! (recall the Comparison)
- Results very bad with this simple choice.

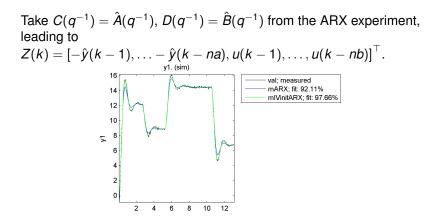
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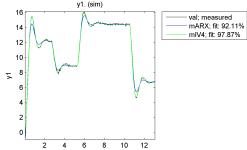
Result with ARX-model instruments



Conclusion: IV obtains better results. This is because the disturbance is colored, and IV can deal effectively with this case (whereas ARX cannot – but it still provides a useful starting point for IV).

model = iv4(id, [na, nb, nk]);

Implements an algorithm that generates near-optimal instruments.



Conclusion: Virtually the same performance as ARX instruments.

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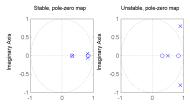
Assumptions

Assumptions (simplified)

- The disturbance $v(k) = H(q^{-1})e(k)$ where e(k) is zero-mean white noise, and $H(q^{-1})$ is a transfer function satisfying certain conditions.
- The input signal u(k) has a sufficiently large order of PE and does not depend on the disturbance (the experiment is open-loop).
- So The real system is stable and *uniquely* representable by the model chosen: there exists exactly one θ_0 so that polynomials $A(q^{-1}; \theta_0)$ and $B(q^{-1}; \theta_0)$ are identical to those of the real system.
- Matrix E $\{Z(k)Z^{\top}(k)\}$ is invertible.

Discussion of assumptions

- Assumption 1 shows the main advantage of IV over PEM: the disturbance can be colored.
- Assumptions 2 and 3 are not very different from those made by PEM. Stability of a discrete-time system requires its poles to be strictly inside the unit circle:



Question: Why is the experiment not allowed to be closed-loop?

• Assumption 4 is required to solve the linear system, and given an input with sufficient order of PE boils down to an appropriate selection of instruments (e.g. not repeating the same delayed input u(k - i) twice).

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Guarantee

Theorem 1

As the number of data points $N \to \infty$, the solution $\hat{\theta}$ of IV estimation converges to the true parameter vector θ_0 .

Remark: This is a consistency guarantee, in the limit of infinitely many data points.

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Possible extensions

- Multiple-input, multiple-output systems.
- Larger-dimension instruments Z than parameter vectors θ with other modifications, called extended IV methods.
- Identification of systems operating in closed loop: next

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Motivation

In practice, systems must often be controlled, because when they operate on their own, in open loop:

- They would be unstable
- Safety or economical limits for the signals would not be satisfied

This means that u(k) is computed using feedback from y(k): the system operates in closed loop

Closed-loop identification

However, most of the techniques that we studied assume the system functions in open loop! For instance, IV guarantees require (among other things):

• ...

• The input signal *u*(*k*) does not depend on the disturbance (the experiment is open-loop)

...

Removing this condition leads to **closed-loop identification**.

Several techniques can be modified for this setting, notably including prediction error methods.

Here, we will focus on IV methods since they are easy to modify.

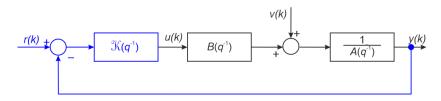
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Closed-loop IV structure



$$A(q^{-1})y(k) = B(q^{-1})u(k) + v(k)$$
$$u(k) = \mathcal{K}(q^{-1})(r(k) - y(k))$$

where $\mathcal{K}(q^{-1})$ is the transfer function of the controller, and r(k) is a reference signal

Therefore, u(k) dynamically depends both on the reference signal and on the system output



The open-loop condition will of course fail. Let us dig deeper into it. The underlying reason for which we needed the loop open was to make the parameter errors:

$$\widehat{\theta} - \theta_0 = \left[\frac{1}{N}\sum_{k=1}^N Z(k)\varphi^\top(k)\right]^{-1} \left[\frac{1}{N}\sum_{k=1}^N Z(k)v(k)\right]$$

equal to zero, leading to a good model. For this, we require:

- $E \{Z(k)v(k)\}$ zero.
- $E \{Z(k)\varphi^{\top}(k)\}$ invertible.

With the usual IV choices, computed based on u (which now depends on y and hence on v), the first condition would fail.

The vector of IVs Z(k) is not allowed to depend on u(k) anymore. Idea: make it a function of r(k)!

Then:

- E {*Z*(*k*)*v*(*k*)} will naturally be zero, since we are the ones generating the reference *r*, independently from the disturbance *v*
- We can make E {Z(k)φ^T(k)} invertible by ensuring the IVs are good (e.g. no linear dependence), and that the reference *r* has a sufficiently high order of PE

Example choices of IVs

Simplest idea – include in *Z* the appropriate number of delayed reference values:

$$Z(k) = [r(k-1), r(k-2), \dots r(k-na-nb)]^{\top}$$

Slightly generalized to linear combinations of these values:

$$Z(k) = \mathbf{F} \cdot [r(k-1), r(k-2), \dots r(k-na-nb)]^{\top}$$

where F is invertible. The simple case is recovered by taking F the identity matrix.

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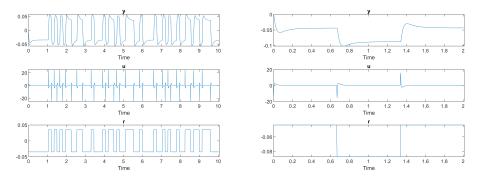
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Experimental data

Identification left, and validation right:



Similarly to the open-loop case, the system has order 2 and the disturbance is colored (does not obey the ARX model structure).

However, now the input is generated by a controller based on the reference signal *r*, which is a PRBS.

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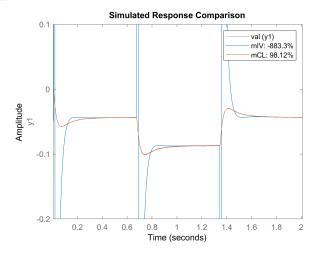
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Results



- Regular IV with ARX instruments: fails.
- Closed-loop IV using *r* to generate instruments: works.



- Objective: combine simplicity of ARX linear regression with generality of PEM disturbance *v*
- Examined in-depth why ARX fails for colored disturbance v
- Solution: replace regressors φ (at strategic places in equations) by *instrumental variables Z* that do not depend on y
- Several ways to compute Z from u only
- Solution quality dependent on Z, may even be unstable
- Matlab example
- Further generalizing Z to depend only on reference r allows IV to work in closed-loop
- Matlab example for closed-loop identification