

# System Identification

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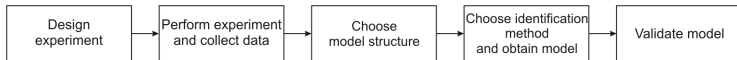
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# Part VI

## Input signals

# Motivation



**Choosing inputs** is the core of experiment design

All identification methods require inputs to satisfy certain conditions, for example:

- Transient analysis requires step or impulse inputs
- Correlation analysis preferably works with white-noise input
- ARX requires “sufficiently informative” inputs

# Plan

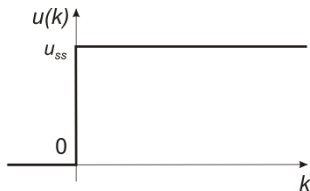
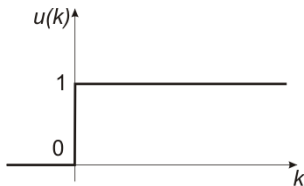
In this part we:

- **Revisit** some types of input signals that were already used
- Describe a few **new types of input signals**
- Discuss **choices and properties** of input signals important for system identification
- **Characterize** the signals discussed using the properties introduced

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# Step input



Left: Unit step:

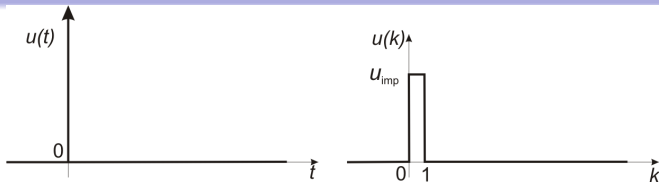
$$u(k) = \begin{cases} 0 & k < 0 \\ 1 & k \geq 0 \end{cases}$$

Right: Step of arbitrary magnitude:

$$u(k) = \begin{cases} 0 & k < 0 \\ u_{ss} & k \geq 0 \end{cases}$$

**Remark:** These are discrete-time reformulations of the continuous-time step variants.

# Impulse input



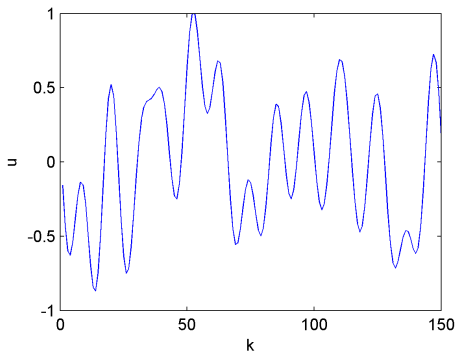
Recall that in discrete time, we cannot freely approximate the ideal impulse (**left**), since the signal can only change values at the sampling instants.

**Right:** Discrete-time impulse realization:

$$u(k) = \begin{cases} u_{\text{imp}} & k = 0 \\ 0 & \text{otherwise} \end{cases}$$

- When  $u_{\text{imp}} = \frac{1}{T_s}$ , the integral of the signal is 1 and we get an approximation of the continuous-time impulse.
- When  $u_{\text{imp}} = 1$  (e.g. in correlation analysis), we get a “unit” discrete-time impulse.

# Sum of sines

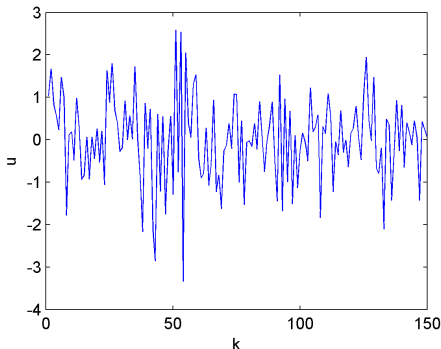


$$u(k) = \sum_{j=1}^m a_j \sin(\omega_j k + \varphi_j)$$

- $a_j$ : amplitudes of the  $m$  component sines
- $\omega_j$ : frequencies,  $0 \leq \omega_1 < \omega_2 < \dots < \omega_m \leq \pi$
- $\varphi_j$ : phases



# White noise



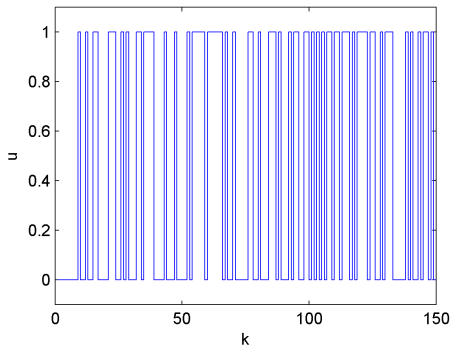
Recall zero-mean white noise: mean 0, different steps uncorrelated.

In the figure, values were independently drawn from a zero-mean Gaussian distribution.

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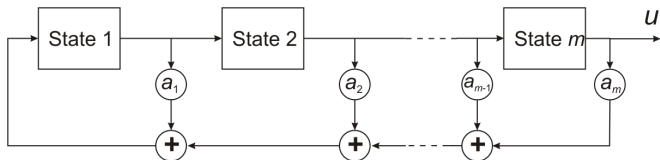
# Pseudo-random binary sequence (PRBS)



A signal that switches between two discrete values, generated with a specific algorithm.

Interesting because it approximates white noise, and so it inherits some of the useful properties of white noise (formalized later).

# PRBS generator



PRBS can be generated with a **linear shift feedback register** as in the figure. All signals and coefficients are binary (the states are bits).

At each discrete step  $k \geq 0$ :

- State  $x_i$  transfers to state  $x_{i+1}$ .
- State  $x_1$  is set to the modulo-two addition of states on the feedback path (if  $a_i = 1$  then  $x_i$  is added, if  $a_i = 0$  then it is not).
- Output  $u(k)$  is collected at state  $x_m$ .

**Remark:** such a feedback register is easily implemented in hardware.

# Modulo-two addition

Formula/truth table of modulo-two addition:

$$p \oplus q = \begin{cases} 0 & \text{if } p = 0, q = 0 \\ 1 & \text{if } p = 0, q = 1 \\ 1 & \text{if } p = 1, q = 0 \\ 0 & \text{if } p = 1, q = 1 \end{cases}$$

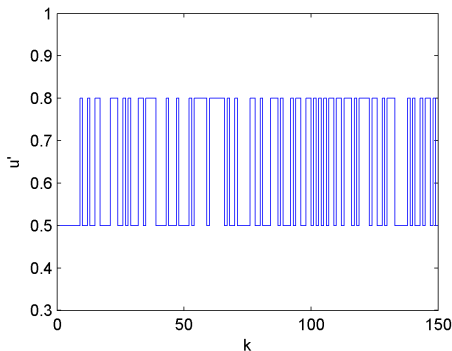
...also known as XOR (eXclusive OR)

# Arbitrary-valued PRBS

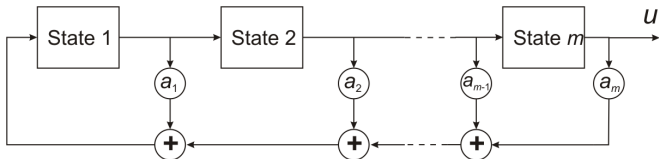
To obtain a signal  $u'(k)$  taking values  $b, c$  instead of 0, 1, shift & scale the original signal  $u(k)$ :

$$u'(k) = b + (c - b)u(k)$$

Example for  $b = 0.5$ ,  $c = 0.8$ :



# State space representation



$$x_1(k+1) = a_1 x_1(k) \oplus a_2 x_2(k) \oplus \dots \oplus a_m x_m(k)$$

$$x_2(k+1) = x_1(k)$$

$$\vdots$$

$$x_m(k+1) = x_{m-1}(k)$$

$$u(k) = x_m(k)$$

$x(k) = [x_1(k), \dots, x_m(k)]^T$  compactly denotes the state vector of  $m$  variables (bits)

# State space representation: matrix form

$$x(k+1) = \begin{bmatrix} a_1 & a_2 & \dots & a_{m-1} & a_m \\ 1 & 0 & \dots & 0 & 0 \\ 0 & 1 & \dots & 0 & 0 \\ \vdots & & & & \\ 0 & 0 & \dots & 1 & 0 \end{bmatrix} \otimes x(k) =: A \otimes x(k)$$

$$u(k) = [0 \ 0 \ \dots \ 0 \ 1]x(k) =: Cx(k)$$

where  $k \geq 0$ , and  $\otimes$  symbolically indicates that the additions in the matrix product are performed modulo 2.



# Period of PRBS

- The PRBS algorithm is deterministic, so the current state  $x(k)$  fully determines the future states and outputs
- ⇒ **Period** (number of steps until sequence repeats) at most  $2^m$
- The identically zero state is undesirable, as the future sequence would always remain 0
- ⇒ Maximum practical period is  $P = 2^m - 1$

A PRBS with period  $P = 2^m - 1$  is called **maximum-length PRBS**.

Such PRBS have interesting characteristics, so they are preferred in practice.

# Maximum-length PRBS

The period is determined by the feedback coefficients  $a_i$ .

The following coefficients must be 1 to achieve maximum length (all others 0):

$m$	Max period $2^m - 1$	Coefficients equal to 1
3	7	$a_1, a_3$
4	15	$a_1, a_4$
5	31	$a_2, a_5$
6	63	$a_1, a_6$
7	127	$a_1, a_7$
8	255	$a_1, a_2, a_7, a_8$
9	511	$a_4, a_9$
10	1023	$a_3, a_{10}$

Other working combinations of coefficients exist, and coefficients for larger  $m$  can be found in the literature.

# Matlab function

```
u = idinput(N, type, [], [b, c]);
```

## Arguments:

- 1 **N**: signal length (number of discrete steps).
- 2 **type**: signal type, a string. Relevant for us: 'prbs' for PRBS, 'rgs' for white Gaussian noise, 'sin' for multisine.
- 3 **Third argument**: the frequency band of the inputs (can be left at its default, empty matrix).
- 4 **[b, c]**: the range (lower and upper limits) of the signal. For Gaussian noise, [b, c] is instead the one-standard-deviation interval below and above the mean.

Remark: **N** can be configured to generate multiple-input signals (see the Matlab documentation for details).

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# Choice of input shape

Some identification methods require specific types of inputs:

- Transient analysis requires step or impulse inputs.
- Correlation analysis preferably works with white-noise input.

Rule of thumb: input shapes, including characteristics like amplitude, should be chosen to be representative for the typical operation of the system

# Choice of input amplitude

Amplitude (+/-)



- Range of allowed inputs typically constrained by system operator, due to safety or cost concerns
- Even if allowed, overly large inputs may take the system out of its zone of linearity and lead to poor performance of linear identification
- But too small inputs will lead to signals dominated by noise and disturbance

# Choice of sampling interval



For nearly all methods, we work in discrete time so we must choose a sampling interval  $T_s$

- Too large intervals will not model the relevant dynamics of the system. Initial idea: 10% of the smallest time constant
- Too small intervals will lead to overly large effects of noise and disturbance
- When in doubt, take  $T_s$  smaller

Due to Nyquist-Shannon, we know that signals cannot be recovered above frequency  $1/(2T_s)$ , so to mitigate noise and other effects it is useful to pass the outputs (and inputs, if measured) through a low-pass filter that eliminates higher frequencies

# Mean and covariance

Given a random signal  $u(k)$ , its mean and covariance are defined:

$$\begin{aligned}\mu &= \text{E} \{u(k)\} \\ r_u(\tau) &= \text{E} \{[u(k + \tau) - \mu][u(k) - \mu]\}\end{aligned}$$

Notes:

- Recall mean and variance of random variables
- The same covariance function  $r_u(\tau)$  was used in correlation analysis, where we assumed the signal is zero-mean
- Zero-mean signals may work better even for other methods, like ARX



# Mean and covariance: deterministic signal

When the signal is deterministic (e.g. PRBS), the mean and covariance are redefined as:

$$\mu = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k)$$

$$r_u(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} [u(k + \tau) - \mu][u(k) - \mu]$$

**Note:**  $\lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} \cdot$  is the same as  $E\{\cdot\}$  for a (well-behaved) random signal.

## Persistent excitation

Even methods that do not fix the input shape make requirements on the inputs: e.g. for ARX we required that  $u(k)$  is “sufficiently informative”, without making that property formal

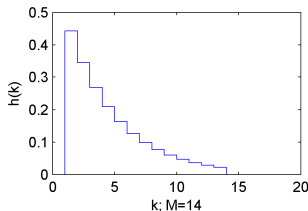
This condition can be precisely stated in terms of a property called **persistence of excitation**

# Persistent excitation: Motivating example

We develop an *idealized* version of correlation analysis. This is only an intermediate motivating step, and the property is useful in many identification algorithms.

Finite impulse response (FIR) model:

$$y(k) = \sum_{j=0}^{M-1} h(j)u(k-j) + v(k)$$



# Correlation analysis: Covariances

Assuming  $u(k)$ ,  $y(k)$  are zero-mean, so the means do not need to be subtracted:

$$r_u(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k + \tau)u(k)$$
$$r_{yu}(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} y(k + \tau)u(k)$$

In practice covariances must be estimated from finite datasets, but here we work with their ideal values (since this is only a motivating example, which we do not actually implement).

# Correlation analysis: Identifying the FIR

Taking  $M$  equations to find the FIR parameters, we have:

$$\begin{bmatrix} r_{yu}(0) \\ r_{yu}(1) \\ \vdots \\ r_{yu}(M-1) \end{bmatrix} = \begin{bmatrix} r_u(0) & r_u(1) & \dots & r_u(M-1) \\ r_u(1) & r_u(0) & \dots & r_u(M-2) \\ \vdots & \vdots & \ddots & \vdots \\ r_u(M-1) & r_u(M-2) & \dots & r_u(0) \end{bmatrix} \cdot \begin{bmatrix} h(0) \\ h(1) \\ \vdots \\ h(M-1) \end{bmatrix}$$

We are allowed to take a square system (number of equations equal to number of parameters) because we are in the idealized, noise-free case, so overfitting is not a concern.

Denote the matrix in the equation by  $R_u(M)$ , the **covariance matrix** of the input.

# Persistent excitation: formal definition

## Definition

A signal  $u(k)$  is **persistently exciting (PE) of order  $n$**  if  $R_u(n)$  is positive definite.

A matrix  $A \in \mathbb{R}^{n \times n}$  is positive definite if  $h^T A h > 0$  for any nonzero vector  $h \in \mathbb{R}^n$ . Note that  $A$  must be nonsingular.

## Examples:

- $\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$  is positive definite. Denote  $h = \begin{bmatrix} a \\ b \end{bmatrix}$ , then  
 $h^T A h = a^2 + b^2$ .
- $\begin{bmatrix} 1 & 2 \\ 2 & 1 \end{bmatrix}$  is not positive definite. Counterexample:  $h = \begin{bmatrix} a \\ -a \end{bmatrix}$ ,  
 $h^T A h = -2a^2$ .

# PE in correlation analysis

If the order of PE is  $M$ , then  $R_U(M)$  is positive definite, hence invertible and the linear system from correlation analysis can be solved to find an FIR of length  $M$ .

So an order  $M$  of PE means that an FIR model of length  $M$  is identifiable ( $M$  parameters can be found).

## General role of PE

Beyond FIR, PE plays a role in *all* parametric system identification methods, including ARX and methods still to be discussed, like prediction error methods and instrumental variable techniques.

A **large enough order of PE** is required to properly identify the parameters.

Typically, the required order is a multiple of (e.g. twice) the number of parameters  $n$  that must be estimated.



# Covariance alternatives

In the sequel we will always use the following, simpler definition:

$$r_u(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k + \tau)u(k)$$

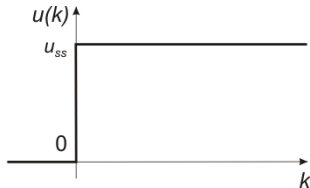
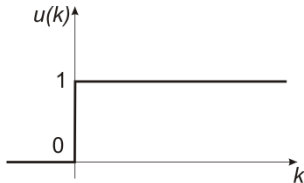
even when  $u$  is nonzero-mean. Even though in that case  $r_u$  is no longer the true covariance in the statistical sense, it is still useful.

When applying the PE condition for nonzero-mean signals, the simplified definition above will lead to an order of PE larger by 1 than the order of PE obtained with the means removed.

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# Step input



Take the more general, non-unit step:

$$u(k) = \begin{cases} 0 & k < 0 \\ u_{ss} & k \geq 0 \end{cases}$$

# Step input: Mean and covariance

Mean and covariance:

$$\mu = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k) = u_{ss}$$

$$r_u(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k + \tau)u(k) = u_{ss}^2$$

Note the signal starts from  $k = 0$ , so the summation is modified (unimportant to the final result).

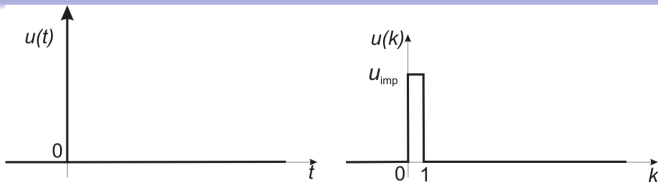
# Step input: Order of PE

Covariance matrix:

$$R_U(n) = \begin{bmatrix} r_u(0) & r_u(1) & \dots & r_u(n-1) \\ r_u(1) & r_u(0) & \dots & r_u(n-2) \\ \vdots & & & \\ r_u(n-1) & r_u(n-2) & \dots & r_u(0) \end{bmatrix} = \begin{bmatrix} u_{ss}^2 & u_{ss}^2 & \dots & u_{ss}^2 \\ u_{ss}^2 & u_{ss}^2 & \dots & u_{ss}^2 \\ \vdots & & & \\ u_{ss}^2 & u_{ss}^2 & \dots & u_{ss}^2 \end{bmatrix}$$

This matrix has rank 1, so a step input is **PE of order 1**.

# Impulse input



Recall discrete-time realization:

$$u(k) = \begin{cases} \frac{1}{T_s} & k = 0 \\ 0 & \text{otherwise} \end{cases}$$

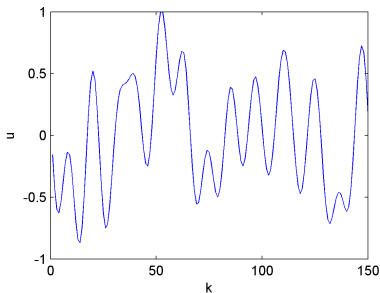
Mean and covariance:

$$\mu = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k) = 0$$

$$r_u(\tau) = \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=0}^{N-1} u(k + \tau)u(k) = 0$$

$\Rightarrow R_u(n)$  matrix of zeros, the impulse is not PE of any order.

# Sum of sines



$$u(k) = \sum_{j=1}^m a_j \sin(\omega_j k + \varphi_j), \quad 0 \leq \omega_1 < \omega_2 < \dots < \omega_n \leq \pi$$

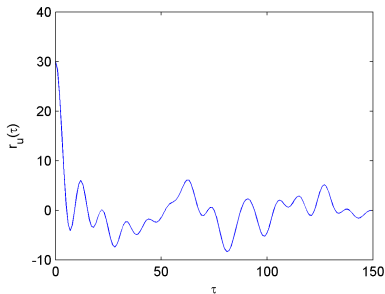
Mean and covariance:

$$\mu = \begin{cases} a_1 \sin(\varphi_1) & \text{if } \omega_1 = 0 \\ 0 & \text{otherwise} \end{cases}$$

$$r_u(\tau) = \sum_{j=1}^{m-1} \frac{a_j^2}{2} \cos(\omega_j \tau) + \begin{cases} a_m^2 \sin^2 \varphi_m & \text{if } \omega_m = \pi \\ \frac{a_m^2}{2} \cos(\omega_m \tau) & \text{otherwise} \end{cases}$$

## Sum of sines (continued)

For the multisine exemplified before, the covariance function is:



A multisine having  $m$  components is **PE of order  $n$**  with:

$$n = \begin{cases} 2m & \text{if } \omega_1 \neq 0, \omega_m \neq \pi \\ 2m - 1 & \text{if } \omega_1 = 0 \text{ or } \omega_m = \pi \\ 2m - 2 & \text{if } \omega_1 = 0 \text{ and } \omega_m = \pi \end{cases}$$



# White noise: Mean and covariance

Take a zero-mean white noise signal of variance  $\sigma^2$ , e.g. drawn from a Gaussian:

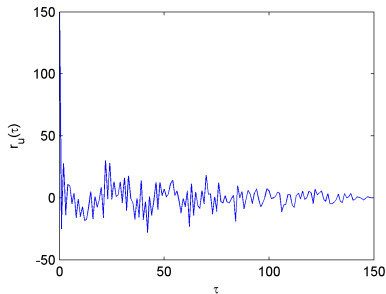
$$u(k) \sim \mathcal{N}(0, \sigma^2) = \frac{1}{\sqrt{2\pi\sigma^2}} \exp\left(-\frac{x^2}{2\sigma^2}\right)$$

Then, by definition:

$$\mu = 0$$
$$r_u(\tau) = \begin{cases} \sigma^2 & \text{if } \tau = 0 \\ 0 & \text{otherwise} \end{cases}$$

# White noise: Covariance example

Covariance function of white noise signal exemplified before:



# White noise: Order of PE

Covariance matrix:

$$R_u(n) = \begin{bmatrix} r_u(0) & r_u(1) & \dots & r_u(n-1) \\ r_u(1) & r_u(0) & \dots & r_u(n-2) \\ \vdots & & & \\ r_u(n-1) & r_u(n-2) & \dots & r_u(0) \end{bmatrix}$$
$$= \begin{bmatrix} \sigma^2 & 0 & \dots & 0 \\ 0 & \sigma^2 & \dots & 0 \\ \vdots & & & \\ 0 & 0 & \dots & \sigma^2 \end{bmatrix} = \sigma^2 I_n$$

where  $I_n$  = the identity matrix, positive definite.

⇒ for any  $n$ ,  $R_u(n)$  positive definite — white noise is **PE of any order**.

## Question

Given the information above, why does correlation analysis prefer white noise to other input signals, in order to identify the FIR?

# PRBS: Mean

Consider a 0, 1-valued, maximum-length PRBS with  $m$  bits:  
 $P = 2^m - 1$ , a large number.

Then its state  $x(k)$  will contain all possible binary values with  $m$  digits except 0.

Signal  $u(k)$  is the last position of  $x(k)$ , which takes value 1 a number of  $2^{m-1}$  times, and value 0 a number of  $2^{m-1} - 1$  times.

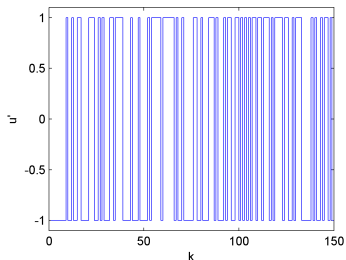
⇒ Mean value:

$$\mu = \frac{0}{P-1} \sum_{k=1}^P u(k) = \frac{1}{P} 2^{m-1} = \frac{(P+1)/2}{P} = \frac{1}{2} + \frac{1}{2P} \approx \frac{1}{2}$$

where the approximation holds for large  $P$ .

# PRBS: Covariance

Consider a zero-mean PRBS, scaled between  $-b$  and  $b$ :



$$u'(k) = -b + 2bu(k)$$

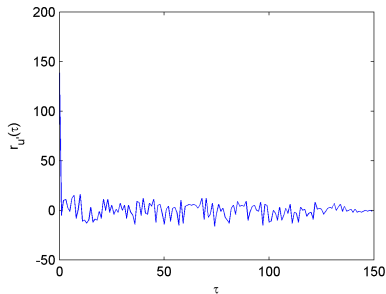
Then:

$$\mu = -b + 2b\left(\frac{1}{2} + \frac{1}{2P}\right) = \frac{b}{P} \approx 0$$

$$r_u(\tau) = \begin{cases} 1 - \frac{1}{P^2} \approx 1 & \text{if } \tau = 0 \\ -\frac{1}{P} - \frac{1}{P^2} \approx -\frac{1}{P} \approx 0 & \text{otherwise} \end{cases}$$

# PRBS: Covariance example

Covariance function of the zero-mean PRBS above:



So, PRBS **behaves similarly to white noise** (similar covariance function). Combined with the ease of generating it, this property makes PRBS very useful in system identification.

# PRBS: Order of PE

A maximum-length PRBS is **PE of exactly order  $P$** , the period (and not larger).

## Exercise

Take a small value of  $P \geq 2$  and, using the formula for the covariance function of the PRBS, show that the PRBS is exactly of PE order  $P$ .

**Hint:** construct  $R_u(n)$  for  $n = P$  and show that it is rank  $P$ , then for  $n > P$  and show it is *still* only of rank  $P$ . This can be done by showing that columns  $P + 1, P + 2, \dots$  are linear combinations of the first  $P$  columns.

# Summary

- Common input signals: step, impulse, multisine, zero-mean white noise, pseudo-random binary sequence
- PRBS details: generation using LFSRs, maximal period
- Choosing input amplitude and sampling period
- Mean and covariance of input signals
- Order of persistent excitation
- Characterizing mean, covariance, and PE order for all common input signals